Electronic Supplementary Material

for

Carbonation rate of alkali-activated concretes and high-volume SCM concretes: a literature data analysis of RILEM TC 281-CCC

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Supplementary Figures S1-S24



Supplementary Figure S1. Carbonation coefficients obtained under conditions approximating natural carbonation (indoor/sheltered) *versus w*/CaO ratio, including the data point for the MK-based AAC. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S2. Carbonation coefficients obtained under conditions approximating natural carbonation (indoor/sheltered) *versus w/*(CaO + MgO_{eq}) ratio. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S3. Carbonation coefficients of the GGBS-based AAC obtained under conditions approximating natural carbonation (indoor/sheltered) *versus w/*(CaO + MgO_{eq}) ratio. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S4. Carbonation coefficients of the BCC obtained under conditions approximating natural carbonation (indoor/sheltered) *versus w/*(CaO + MgO_{eq}) ratio.



Supplementary Figure S5. Carbonation coefficients of the BCC obtained under conditions approximating natural carbonation (indoor/sheltered) versus w/(CaO + MgO_{eq} + Na₂O_{eq} + K₂O_{eq}) ratio.



Supplementary Figure S6. Carbonation coefficients of the BCC obtained under conditions approximating natural carbonation (indoor/sheltered) *versus w/b* ratio.



Supplementary Figure S7. Carbonation coefficients obtained under conditions approximating natural carbonation (indoor/sheltered) *versus w/b* ratio. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S8. Carbonation coefficients obtained under conditions approximating natural carbonation (indoor/sheltered) *versus* binder content. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S9. Carbonation coefficients obtained under conditions approximating natural carbonation (indoor/sheltered) *versus* paste content. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S10. Carbonation coefficients of the AAC obtained under conditions approximating natural carbonation (indoor/ sheltered) *versus* activator content. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S11. Carbonation coefficients of the AAC obtained under conditions approximating natural carbonation (indoor/ sheltered) *versus* activator modulus (molar SiO₂/M₂O ratio). *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S12. Carbonation coefficients of the BCC obtained under conditions approximating natural carbonation (indoor/sheltered) *versus* Portland clinker content.



Supplementary Figure S13. Carbonation coefficients obtained with a CO₂ concentration of 1 % (accelerated conditions) *versus w*/CaO ratio. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S14. Carbonation coefficients obtained with a CO_2 concentration in the range 3–5 % (accelerated conditions) *versus w*/CaO ratio.



Supplementary Figure S15. Carbonation coefficients obtained with a CO₂ concentration in the range 10–100 % (accelerated conditions) *versus w*/CaO ratio.



Supplementary Figure S16. Carbonation coefficients obtained with a CO_2 concentration of 1 % (accelerated conditions) *versus w/*(CaO + MgO_{eq}) ratio. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S17. Carbonation coefficients obtained with a CO_2 concentration in the range 3–5 % (accelerated conditions) *versus w/*(CaO + MgO_{eq}) ratio.



Supplementary Figure S18. Carbonation coefficients obtained with a CO_2 concentration in the range 10–100 % (accelerated conditions) *versus w/*(CaO + MgO_{eq}) ratio.



Supplementary Figure S19. Carbonation coefficients obtained with a CO₂ concentration of 1 % (accelerated conditions) *versus w/b* ratio. *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S20. Carbonation coefficients obtained with a CO_2 concentration in the range 3–5 % (accelerated conditions) *versus w/b* ratio.



Supplementary Figure S21. Carbonation coefficients obtained with a CO_2 concentration in the range 10–100 % (accelerated conditions) *versus w/b* ratio.



Supplementary Figure S22. Carbonation coefficients obtained with a CO₂ concentration of 1 % (accelerated conditions) *versus* activator modulus (molar SiO₂/M₂O ratio). *Error bars* represent the estimated standard deviations of the results obtained in the round robin testing programme by RILEM TC 247-DTA.



Supplementary Figure S23. Carbonation coefficients obtained with a CO_2 concentration in the range 3–5 % (accelerated conditions) *versus* activator modulus (molar SiO₂/M₂O ratio).



Supplementary Figure S24. Carbonation coefficients obtained with a CO_2 concentration in the range 10–100 % (accelerated conditions) *versus* activator modulus (molar SiO₂/M₂O ratio).