



## Impact of catalyst layer morphology on the operation of high temperature PEM fuel cells



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### ABSTRACT

Electrochemical impedance spectroscopy (EIS) is a well-established method to analyze a polymer electrolyte membrane fuel cell (PEMFC). However, without further data processing, the impedance spectrum yields only qualitative insight into the mechanism and individual contribution of transport, kinetics, and ohmic losses to the overall fuel cell limitations. The distribution of relaxation times (DRT) method allows quantifying each of these polarization losses and evaluates their contribution to a given electrocatalyst's depreciated performances. We coupled this method with a detailed morphology study to investigate the impact of the 3D-structure on the processes occurring inside a high-temperature polymer electrolyte membrane fuel cell (HT-PEMFC). We tested a platinum catalyst (Pt/C), a platinum-cobalt alloy catalyst (Pt<sub>3</sub>Co/C), and a platinum group metal-free iron-nitrogen-carbon (Fe-N-C) catalyst. We found that the hampered mass transport in the latter is mainly responsible for its low performance in the MEA (along with its decreased intrinsic performances for the ORR reaction). The better performance of the alloy catalyst can be explained by both improved mass transport and a lower ORR resistance. Furthermore, single-cell tests show that the catalyst layer morphology influences the distribution of phosphoric acid during conditioning.

### 1. Introduction

PEMFCs have been extensively researched over the last years [1,2]. They hold promises to become a clean and compact electricity source for stationary to mobile applications. However, to achieve this goal, several challenges should be resolved. They range from managing the water at high current densities to the need for high purity gases, as impurities significantly affect the PEMFC performance, increasing their operating costs [3,4]. Operating PEMFCs above 120 °C overcomes many of these disadvantages as it eliminates liquid water from the system, therefore simplifying the water management, which reduces the complexity of the system.

Furthermore, the electrode kinetics are to be potentially faster. This effect is slightly compromised by the change in Gibbs free energy, which decreases linearly with increasing temperature. The elevated temperatures enable the system to run on steam reformates, as impurities (e.g. CO up to 3% in the anode gas stream) do not drastically impact the cell performance [5,6].

High-temperature PEMFCs (HT-PEMFCs) are usually operated at 160 °C. The proton conductivity of the conventional membrane, Nafion®, is reduced due to insufficient membrane hydration, induced by the absence of liquid water. Thus, HT-PEMFCs utilize a different proton-conducting membrane, namely phosphoric acid (H<sub>3</sub>PO<sub>4</sub>)-doped polybenzimidazole (PBI). In the catalyst layer, the liquid phosphoric acid conducts the protons to the reaction sites. Thus, the distribution of phosphoric acid inside the catalyst layer is vital for the triple-phase boundary and is key for the performance of the cell. Although various groups studied this issue in the past decade, it still requires a better understanding to achieve dynamic control of the triple-phase boundary [7–11]. The performance of the cell is further influenced by the catalytic activity of the cathode catalyst, where the oxygen reduction reaction (ORR) occurs. To improve its rate, platinum electrocatalysts (e.g. carbon-supported Pt nanoparticles, the state-of-the-art PEMFC cathode electrocatalyst) are often replaced by platinum-alloys, aiming to increase the ORR intrinsic activity through the strain-ligand and/or coarsening effects to reduce thereby the amount of the expensive platinum inside a

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fuel cell [12–15]. Alloying platinum with 3d transition metal, such as nickel or cobalt, has proven to deliver the most significant improvement. For example, the Pt<sub>3</sub>Co particles exhibit a Pt-rich surface layer with a reduced interatomic distance, which results in a modification of the Pt electronic structure and, thus, a decreased binding strength of the oxygen intermediate onto the catalytic surface. Furthermore, the non-noble part of the catalyst leaches out during operation, creating a rough catalyst surface. All these increase the reaction rate and the performance of the cell [15,16].

Further alternatives for conventional platinum catalysts are carbonaceous materials doped with atomically dispersed catalyst sites, often referred to as iron-nitrogen-carbon (Fe–N–C), which present the advantage being free of expensive and rare platinum group metals (PGMs). The electrode structure of the PGM-free catalyst has been thoroughly investigated by several groups [17–21]. They consist of a carbonaceous structure, composed of graphitic and amorphous domains with various types of moieties, either metal-free (e.g. pyridinic nitrogen, pyrrolic nitrogen, graphitic nitrogen, etc.) or M–N<sub>x</sub>, the activity of which greatly depends on their coordination and their position in the carbon network. It is, however, often accepted that the M–N–C electrocatalysts should be designed while considering the M–N<sub>4</sub> moieties as the primary catalytic site for the ORR in PEMFCs, as they are usually found *in-plane*, in the mesopores and thus easily accessible, even in a solid electrolyte [22], by opposition to sites (e.g. Fe–N<sub>2+2</sub>, N–Fe–N<sub>2+2</sub>) which are present in the micropores and thus, exhibit low accessibility [21,23–26]. Notably, the oxygen diffusion in this type of catalyst is inhibited. Increased back-pressure significantly boosts the performance of the cell, which indicates a mass transport issue [27]. During their operation in an HT-PEMFC, the reactants and reaction products need to be transported to and from the *in-plane* defects and, thus, navigate through the Fe–N–C complex network of meso (2–50 nm) and microporosities (<2 nm), hence requiring those defects to be in contact with the proton carrier, the viscous H<sub>3</sub>PO<sub>4</sub>. This process can be expected to inhibit the utilization of the catalyst sites, especially when considering that in conventional PEMFCs, Nafion® micelles with an average micelle size of 30 nm will also prevent proton transport in the smallest porosities [28]. This specific aspect is expected to be far less of a limitation when addressing PGM-group electrocatalysts, as the nanoparticles, ranging from 2 to 3 nm for pure-Pt and Pt-alloys to several dozens of nm for complex nanostructures, (e.g. Pt-based hollow nanoparticles [29], nanoframes [30], octahedra [31]) are far less likely to anchor/nucleate in the smallest porosities and are thus readily available for the reaction, exhibiting a lower transport resistance. However, the catalyst layer morphology plays a role in mass transport (MT) and Oxygen reduction reaction (ORR). Therefore it decisively influences the performance of the cell.

MT also includes the transport of protons to the reaction sites. Thus, the reaction sites need to be in contact with phosphoric acid to contribute to cell performance. An ideal wetting of the carbon support would include the smallest porosities, no flooding, and a thin film over the whole carbon support to optimize MT to the active sites. The proton conduction in the cathode is visible in the DRT spectrum of a HT-PEMFC [32]. Thus, different wetting behavior in catalysts with varying pore sizes can be observed using DRT.

X-ray tomographic methods were applied to investigate water transport in conventional PEMFCs to resolve MT phenomena in conventional PEMFCs [33]. These methods have been optimized over the years, and operando X-ray micro-computed tomography has been used to understand the water transport in Fe–N–C catalysts [34,35]. As the resolution of these techniques is insufficient to resolve the phosphoric acid distribution in nanometer-scaled pores of HT-PEMFC catalyst layers, operando X-ray micro-computed tomography is limited to a larger scale transport ways, such as cracks in the layered structure [36].

Several electrochemical impedance spectroscopy (EIS) studies on HT-PEMFCs were discussed in the literature [6,37–40]. They all found that hampered mass transport (MT) is responsible for severe polarization losses of the cell. To separate and quantify the different processes

occurring inside the HT-PEMFC (*i.e.* reactant transport through the membrane or the porous network, charge transfer, *etc.*), we implemented the distribution of relaxation times (DRT) method, hence increasing our understanding of the cell's limitations. DRT has also been applied to analyze impedance spectra of other electrochemical systems such as solid oxide fuel cells by Schichlein et al. [41] and lithium-ion batteries [42]. Cuicci and Chen [43] developed a model to investigate the impedance spectra of PEMFCs, and Heinzmann et al. evaluated a conventional PEMFC [44]. A comprehensive overview of the development and application of the DRT method is presented by Dierickx et al. [45].

In our study, we allocated characteristic peaks of the spectrum to specific processes in a HT-PEMFC by varying the operating parameters of the cell. A typical fingerprint pattern is found for HT-PEMFCs equipped with various catalysts, which allows a direct comparison between cells [46]. Yezerka et al. [47] applied DRT analysis to artificially corroded catalysts to identify side-reactions. The spectrum of a low-temperature PEMFC shows unique characteristics different from those of a HT-PEMFC [44]. They mainly relate to the different morphology of the catalyst layer (*i.e.* higher thickness, PTFE as a binder instead of Nafion®) and the presence of phosphoric acid [32]. In this work, single-cell tests were performed with MEAs using various electrocatalysts. They belong to different groups: state-of-the-art Pt/C, Pt<sub>3</sub>Co/C, and Fe–N–C. The cells exhibit a substantial performance gap, which could be explained by analyzing the impedance spectra coupled with DRT analysis. Furthermore, the results were linked to the morphology and the pore size distribution of the catalyst layers.

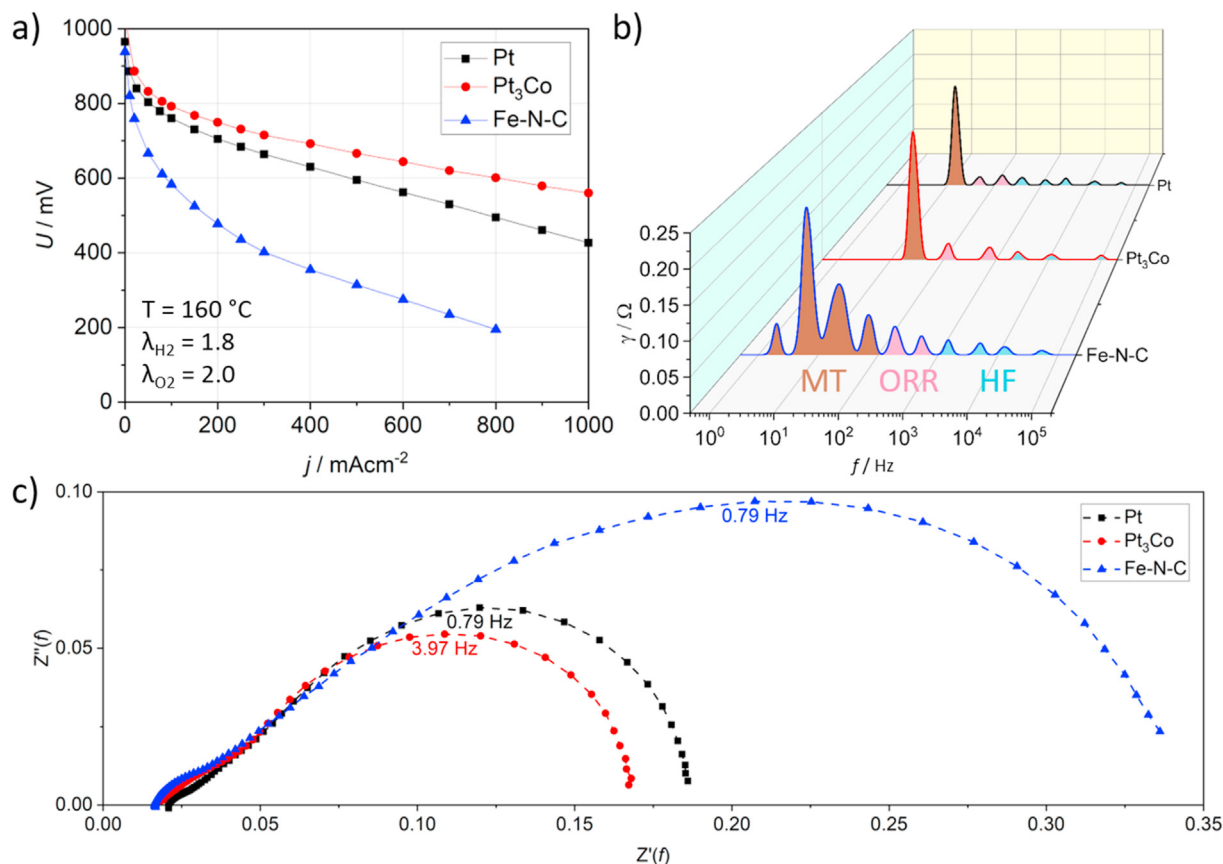
## 2. Experimental

### 2.1. Synthesis of the Fe–N–C catalyst

The Fe–N–C electrocatalysts were synthesized using the sacrificial support method (SSM). Namely, the precursors (*i.e.* Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O and Nicarbazine, from Sigma, LM-150, from Cabot, Ox-50, from Evonik and home-made Stöber Spheres) were mixed by wet impregnation overnight, before drying at 45 °C, a ball-milling (30 min, 45 Hz) and pyrolysis at 975 °C, for 45 min, under 7% H<sub>2</sub>. The pyrolyzed material was ball-milled (30 min, 45 Hz) and etched in HF for four days to remove the silica (LM-150, Ox-50, and Stöber Spheres). Following the etching, the material was washed to neutral pH, dried, and pyrolyzed a second time, at 950 °C for 30 min, under 10% NH<sub>3</sub>. The resulting electrocatalyst was ball-milled (1 h, 45 Hz) and used for the following characterizations.

### 2.2. Gas diffusion electrode fabrication

The fabrication process of the GDE influences catalyst distribution and needs to be optimized to obtain optimum performance [48,49]. Catalyst ink was prepared by mixing catalyst powder (Pt: 20 wt-% on Vulcan XC-72, Heraeus®; Pt<sub>3</sub>Co: 30 wt-% on carbon black (undisclosed details), Tanaka; Fe–N–C: see above), IPA, and deionized water. The weight ratio of catalyst powder, IPA, and deionized water was 1:16:16. A 60 wt-% PTFE dispersion (TF 5060 GZ, 3 M™ Dyneon™) was added as a binder (7 wt-% of the dry electrode), and the dispersion was stirred for 2 h using a magnetic stirrer with a stir bar. The ink was subsequently spray-coated layer by layer onto a commercially available gas diffusion layer with a microporous coating (H2315–C2, Freudenberg®) at a temperature of 80 °C to dry the solvents during the coating process. The ink was sprayed using an airbrush system at an exuding pressure of 2 bar. The metal loading amounts to 1 mg<sub>Pt</sub> cm<sup>–2</sup> in the Pt catalyst and 1 mg<sub>M</sub> cm<sup>–2</sup> (M = metal) in the case of the Pt<sub>3</sub>Co catalyst. The Fe–N–C catalyst loading was 3 mg cm<sup>–2</sup> (number represents the total weight of the catalyst). Catalyst loading was determined by weighing the dry gas diffusion electrode (GDE) after spray-coating. A more in-depth explanation of the GDE fabrication process was provided by Mack et al. [50,51]. The GDEs were cut into squares with a surface area of 4 cm<sup>2</sup> and laid on top of a stainless steel bipolar plate with serpentine gas flow channels with a



**Fig. 1.** Performance evaluation by all applied techniques of three investigated catalysts types. a) HFR-corrected polarization curves displaying the cell voltage  $U$  versus the applied current density  $j$ . b) distribution of relaxation times spectra. The frequency  $f$  is plotted versus the distribution function  $\gamma$ . c) Nyquist plots (real part  $Z'(f)$  vs. imaginary part  $Z''(f)$ ) of electrochemical impedance at the same operating conditions ( $\lambda_{\text{H}_2} = 1.8$ ,  $\lambda_{\text{O}_2} = 2.0$ ,  $j = 100 \text{ mA cm}^{-2}$ ) for DRT and EIS. Apex frequency for the largest semi-circle is indicated with the label in the respective color. (For interpretation of the references to color in this figure legend, the reader is referred to the Web version of this article.)

width and depth of 1 mm each. The torque applied to eight screws was 2 Nm. They were fit into place by a PTFE gasket with a thickness of 220  $\mu\text{m}$  to ensure that no gas is leaking and preventing cross-over. A PBI membrane (Dapozol® M40, Danish Power Systems) was doped for 14–28 days in concentrated phosphoric acid (85%, Normapur, VWR Chemicals) and sandwiched between the gas diffusion electrodes. In each cell, the anode was a standard Pt electrode with a loading of  $1 \text{ mgPt cm}^{-2}$ . This excess of anode loading was used to ensure that no operational limitations originate from the anode and ensure that the cathodic processes can be resolved without interference.

### 2.3. Cell operation

The conditioning of the assembled cells was achieved by heating them to  $160^\circ\text{C}$  in a nitrogen atmosphere using heat pads and subsequently supplying them with hydrogen ( $\lambda_{\text{H}_2} = 1.8$ ) and air ( $\lambda_{\text{Air}} = 2.0$ ) at ambient pressure ( $\lambda = \text{stoichiometry}$ ). A current of  $100 \text{ mA cm}^{-2}$  was applied during the conditioning to ensure water production, which dilutes the phosphoric acid to facilitate proper acid distribution and to keep the cell voltage at a non-corrosive potential. During activation, polarization curves and impedance spectra were recorded after 2 h and every 24 h. After 120 h, each cell reached (or has already reached) a steady cell voltage, and the activation was finished. After conditioning, operation parameters were changed to monitor the response of the fuel cell. The parameters were in all cases varied at least 30 min before recording an impedance spectrum and a polarization curve to give the system enough time to equilibrate and to ensure that the EIS captures only steady-state phenomena. Where specified, oxygen was chosen as the cathode reactant

gas. The stoichiometry on the cathode side was varied between  $\lambda = 2.0$ , 5.0, and 10.0 for both air and oxygen. The hydrogen stoichiometry was always kept constant at  $\lambda_{\text{H}_2} = 1.8$ .

### 2.4. Electrochemical impedance spectroscopy

Impedance spectra were recorded after an equilibration period of 30 min using a Zahner Zennium (Zahner Elektrik) workstation connected to a Zahner Power Pack 211, which supplied the current. The frequency range over which the data was collected was 100 kHz to 50 mHz, at a rate of 10 points per decade and 6 repetitions for each point. This range successfully captures all frequencies at which fast processes such as the hydrogen oxidation reaction and proton transport, and slow processes such as oxygen diffusion and the oxygen reduction reaction occur.

### 2.5. Distribution of relaxation times analysis

The resulting impedance spectra were further analyzed using the distribution of relaxation times analysis with the open-source toolbox DRTtools [52]. Quantification of each process's contribution to the overall impedance of the cell was achieved by calculating the area under each peak. The attribution of each peak to a process inside the fuel cell has been accomplished by Weiß et al. [37]. The slowest processes (within the frequency range until 50 mHz as mentioned earlier) is attributed to oxygen mass transport (MT) and typically range from 1 Hz to 15 Hz. For Pt and Pt<sub>3</sub>Co catalysts, MT is characterized by one peak that is usually higher than the other peaks. The oxygen reduction reaction (ORR) results in two peaks between 15 Hz and 150 Hz, and typically above 150 Hz, the

high frequency (HF) area is found, which includes the hydrogen oxidation reaction and proton transport in the catalyst layer. The frequency range of a DRT spectrum might shift due to pressure fluctuations or if the time constants of the internal processes vary. The frequency ranges mentioned above are not rigid borders, the latter being described by the peaks in the spectrum more than the values mentioned hereinto. Thus, each cell is rather classified by a fingerprint pattern. DRT spectra of HT-PEMFC are described in more detail in the literature [32,37,46].

## 2.6. Morphology characterization

To investigate the three-dimensional structure of the catalysts, high-resolution sorption measurements (3Flex, Micromeritics®) and high-resolution focussed ion beam scanning electron microscopy (FIB-SEM) tomography were conducted [53]. The nitrogen sorption was used to characterize the pores with a diameter below 100 nm. The device was equipped with a special micropore port and a 0.1 Torr pressure transducer. The samples were outgassed at 160 °C for 4 h. Classical macroscopic theories typically lead to an underestimation of pore sizes in micropores and mesopores [54]. To account for the inaccuracy of BET at low pore diameters, the differential pore surface area was calculated using the Non-Local Density Functional Theory (NLDFT) method with the assumption of cylindrical pore shape. The NLDFT describes the sorption behavior of fluids in the vicinity of curved walls, such as in micropores, on a molecular level and is hence more accurate than macroscopic approaches [55,56]. The NLDFT method used in this work is built into the analysis software 3Flex® of the Micromeritics® device.

FIB-SEM images of the Pt catalyst and the Pt<sub>3</sub>Co catalyst were recorded at Helmholtz-Zentrum Berlin (Zeiss Crossbeam 340 gallium FIB with a Gemini column). The edge length of each voxel amounts to 5 nm in all dimensions, the electrons were accelerated with a voltage of 3 kV, and the secondary electrons were detected. The ablation was achieved with a FIB current of 700 pA. The images were translated into a pore network representing the void phase of the porous carbon flakes, and the pore size distribution was analyzed with a watershed-based algorithm using a code written by Gostick [57]. The pore size distribution was created using the open-source pore network modeling software OpenPNM [58]. A more detailed explanation of this process can be found in the literature [7,8].

## 3. Results and discussion

### 3.1. Normal operation

To understand the connection between all three applied techniques, Fig. 1 presents a comparison of the polarization curves (a), the DRT spectra (b), and the Nyquist plots of all three investigated catalysts (c). Fig. 1a shows the polarization curves of the cells operated with hydrogen ( $\lambda_{\text{H}_2} = 1.8$ ) and oxygen ( $\lambda_{\text{O}_2} = 2.0$ ) as fuel gases. The Pt<sub>3</sub>Co alloy catalyst (red) performs better than the standard Pt catalyst, in agreement with the literature [12–15]. The Fe–N–C performs worse than the PGM-containing catalysts. Without further characterization, it is impossible to determine the cause of the performance differences between the three catalysts. However, the first assumption would be to assess them to the lower intrinsic activity of the Fe–N–C electrocatalysts. The ohmic regions of the

**Table 1**

Resistances obtained from DRT analysis of the three investigated catalysts operating with oxygen at 100 mA cm<sup>-2</sup> and power density at 200 mA cm<sup>-2</sup> after conditioning. The maximum power density has not been reached for these cells at 1000 mA cm<sup>-2</sup>.

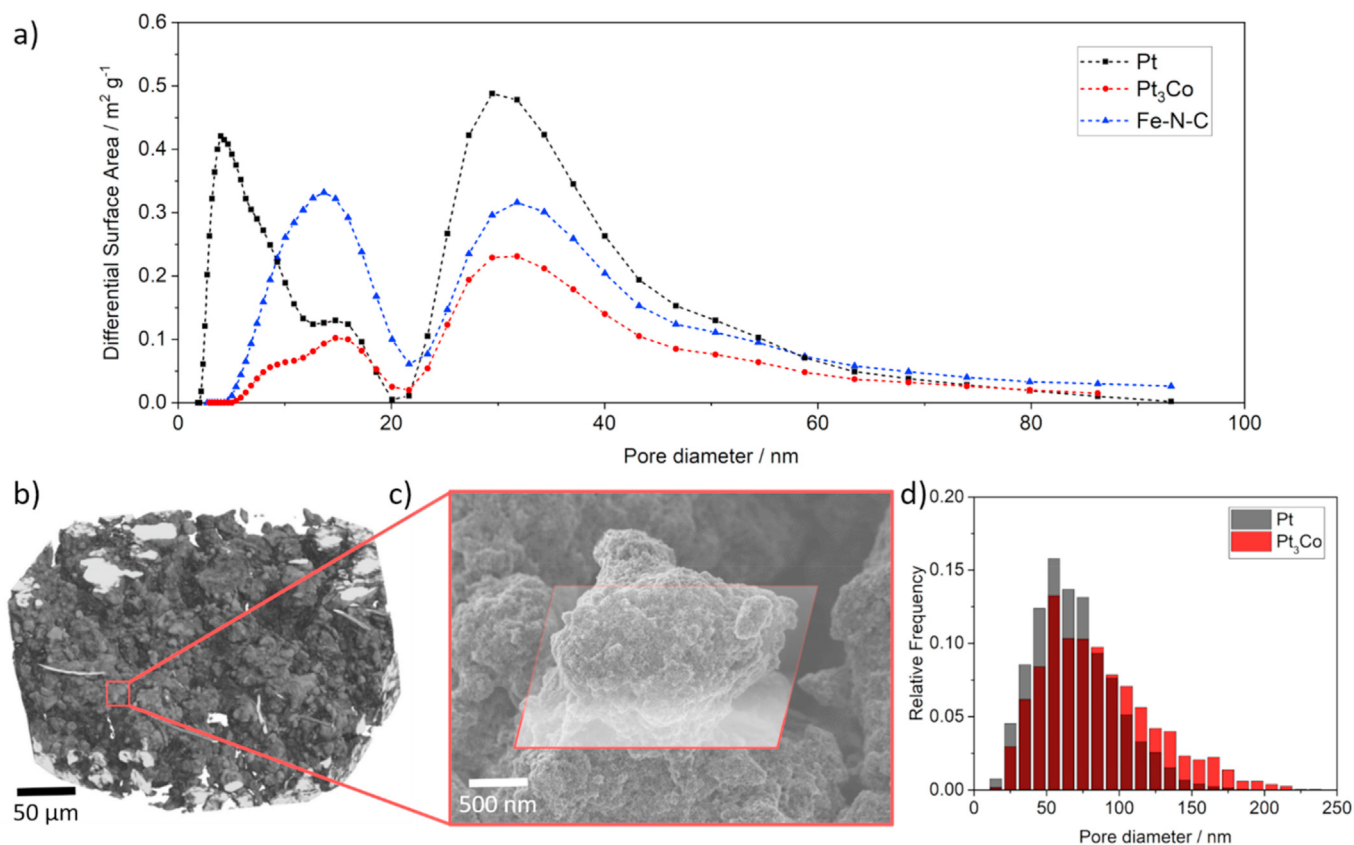
	Pt/C	Pt <sub>3</sub> Co/C	Fe–N–C
Mass transport resistance/mΩ	88.7	26.5	243.7
Oxygen reduction reaction resistance/mΩ	24.2	11.8	61.9
High frequency resistance/mΩ	13.4	13.3	18.4
Power density @ 200 mA cm <sup>-2</sup> /mW cm <sup>-2</sup>	35.3	37.5	23.9

HT-PEMFC typically occur at current densities ( $j$ ) higher than 400 mA cm<sup>-2</sup>, at which the mass transport already affects the performance of the cell. Hence, the ohmic region is expected to be influenced by membrane resistance and oxygen mass transport inside the cell. In our setup for HT-PEMFCs, no typical logarithmic decline of the polarization curve can be observed, even at 2000 mA cm<sup>-2</sup>. Thus, substantial mass transport limitation cannot be excluded solely by the polarization curve.

To determine the exact cause of the performance differences, EIS and subsequent DRT analysis of the impedance spectra was performed. The impedance shown in Fig. 1c displays an increased mid to low frequency resistance for the Fe–N–C catalyst (blue). The cell employing the Pt<sub>3</sub>Co catalyst (red) shows a decreased mid to low frequency resistance compared to the standard Pt cell (black). Minor differences of the high-frequency onset ( $Z''(f) = 0$ ) originate from variations in the membrane resistance. The high-frequency region of the EIS shows similarities between all three catalysts, as it originates from proton conduction in the catalyst layer and the anode, which is the same electrode (1 mgPt cm<sup>-2</sup>) in all cases.

The DRT spectrum (Fig. 1b) exhibits the fingerprint pattern mentioned above for the commercial PGM catalysts with porous carbon powder-based substrates. The pattern for the Pt catalyst (black) shows one dominant mass transport peak at low frequencies (1–15 Hz), followed by two oxygen reduction reaction peaks at medium frequencies (15–150 Hz) and several peaks at higher frequencies (>150 Hz). The shape and allocation of this pattern to the various fuel cell processes are found in greater detail in the literature [32,37]. The same fingerprint is observed in the Pt<sub>3</sub>Co catalyst (red). However, the mass transport peak is narrower, and the second ORR peak is shifted toward higher frequencies (up to 500 Hz). This shift is caused by faster reaction kinetics and is consistent with the observed ORR performance of this catalyst [12–15]. As mentioned earlier, a change of frequencies in the DRT can occur by varying time constants of the respective process. The DRT spectrum of the Fe–N–C shows similar features as the standard cell. We, therefore, assume that the processes occurring in both cells do not differ significantly. The Pt<sub>3</sub>Co system outperforms the standard Pt catalyst, which translates into a smaller Nyquist plot with a higher apex frequency. The apex frequency indicates that the process which is limiting the performance the most (oxygen mass transport) is faster. This fact is confirmed by the more accurate DRT method, in which the MT peak of Pt<sub>3</sub>Co/C occurs at a higher frequency. DRT analysis further shows that the higher performance originates from both the facilitated mass transport (ca. 30% decrease vs. Pt/C) and the improved ORR kinetics (ca. 50% vs. Pt/C) of the alloyed system. The improved MT is surprising at first glance since both platinum-based nanoparticles are supported on carbon black. The improvement might arise from a different morphology of the supports (i.e. Vulcan XC72 for Pt/C vs. undisclosed carbon black support for Pt<sub>3</sub>Co/C). This discrepancy is to be further elaborated in Section 3.2.

The DRT spectrum of the Fe–N–C (blue) catalyst clearly shows a similar fingerprint as the PGM-containing catalysts. Thus, the processes occurring inside this type of catalyst can be assumed to be identical, and the time scales do overlap. Further, the change of the peaks in the DRT spectrum during conditioning (see Fig. S1) indicates that the mass transport regime for this type of catalyst occurs at 1–100 Hz. The peaks describing the oxygen reduction reaction occur at 100–600 Hz. A distinction of the DRT spectrum of the Fe–N–C catalyst is that the low-frequency region of the DRT Fe–N–C catalyst spectrum exhibits multiple peaks, indicating a change of the mass transport process inside the cell. The EIS also does not show a semi-circle at low frequencies, which is why the DRT method fits more than one peak to describe the MT. The low-frequency resistance is dominating for all three catalysts, but this effect is exacerbated for the Fe–N–C catalyst. That indicates that for many catalyst sites, the H<sub>3</sub>PO<sub>4</sub> and oxygen have difficulties accessing them (e.g., in micropores or other small porosities), such as the Fe–N<sub>2+2</sub> or Fe–N<sub>2</sub> sites. This explanation confirms the statement in the introduction that catalyst sites in the micropores are detrimental due to their poor accessibility. Compared to Pt/C and Pt<sub>3</sub>Co/C, the distribution of catalyst



**Fig. 2.** (a) Differential pore surface area from all three catalyst powders obtained from the sorption measurements. (b) Sample 3D X-ray micro-computed tomogram of the catalyst showing the micrometer scale of the catalyst layer. (c) SEM image of the highlighted portion, showing one carbon flake (nanometer scale). The region of interest for FIB-SEM imaging is shown in red. (d) The pore size distribution of nanoscale pores diameters obtained by extracting a pore network from FIB-SEM data [57]. The Pt catalyst is shown in black, the  $\text{Pt}_3\text{Co}$  catalyst is colored in red. (For interpretation of the references to color in this figure legend, the reader is referred to the Web version of this article.)

sites in Fe-N-C [21,23] aggravates the negative influence of a suboptimal impregnation of the electrode by phosphoric acid. As mentioned in the introduction, the Pt and  $\text{Pt}_3\text{Co}$  nanoparticles (2–3 nm) are less likely to anchor or nucleate inside micropores and exhibit much higher accessibility than the micropores sites in Fe-N-C electrocatalysts. The high-frequency resistance of the Fe-N-C catalyst is increased as well, according to both the cell voltage decreases at  $100 \text{ mA cm}^{-2}$  and the EIS/DRT signals, further indicating depreciated kinetics vs. Pt and  $\text{Pt}_3\text{Co}/\text{C}$ . Overall, the hampered mass transport and kinetics for Fe-N-C translates into additional peaks in the DRT spectrum. The quantitative results of the DRT spectrum recorded during regular operation are shown in Table 1. The mentioned limitations, the mass transport and ORR charge transfer resistances, are, for Fe-N-C, increased by a factor of ca. 2.5 vs. Pt/C.

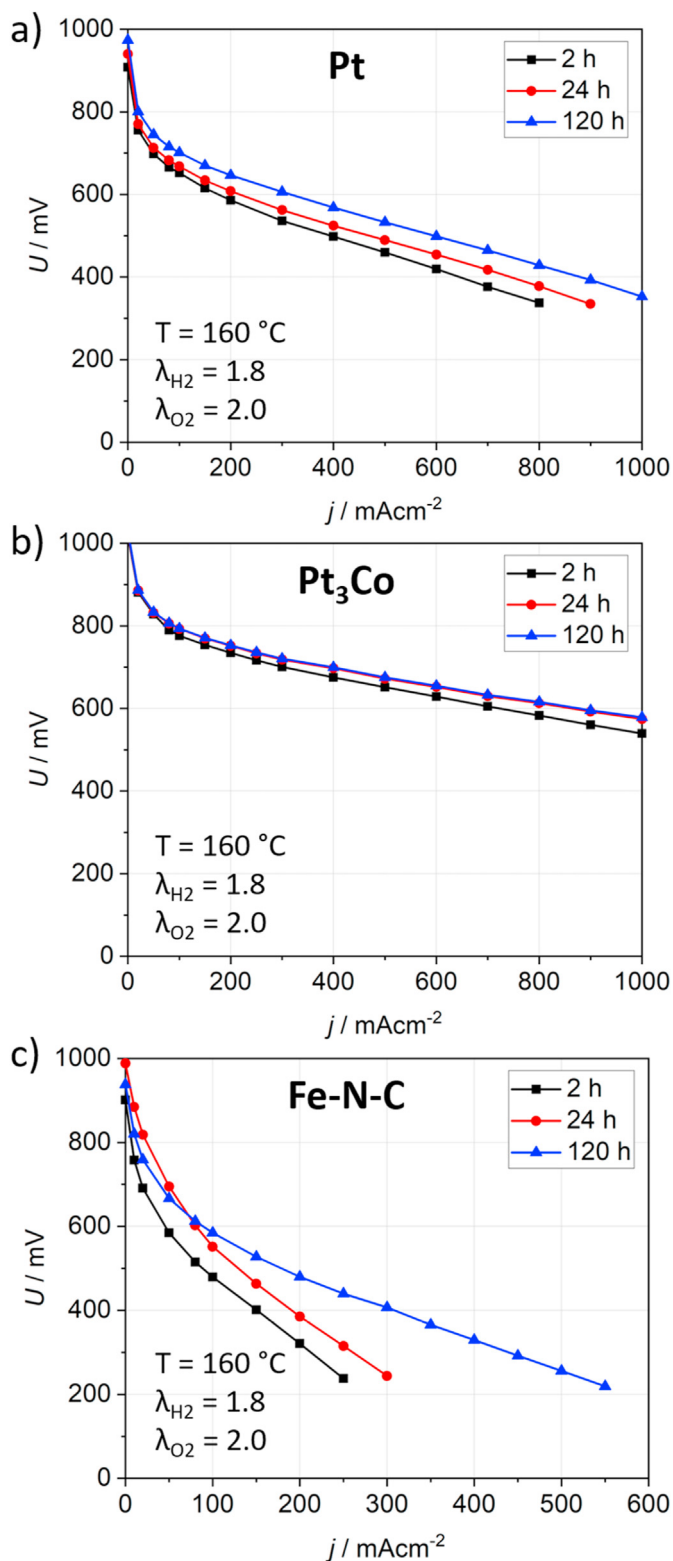
### 3.2. Catalyst layer morphology

Fig. 2a shows the differential pore surface area in the catalyst powders obtained with sorption experiments from 2 nm–93 nm pore diameter. All three catalysts exhibit a hierarchical pore structure with pores below and above 20 nm in diameter and a minimum at 20 nm. The Pt catalyst has the highest fraction of pore surface area below 20 nm (67% of the total surface area) compared to  $\text{Pt}_3\text{Co}$  (44%) and Fe-N-C (61%). We expect slower oxygen diffusion in smaller pores. The DRT analysis confirms that substantially fewer small pores (below 20 nm) of the  $\text{Pt}_3\text{Co}$  catalyst benefit the fuel cell performance by reducing the mass transport resistance, as discussed in Section 3.1. This result further indicates that the catalytic particles located in the smallest pores participate in the reaction, as they contribute to the EIS. Consequently,  $\text{H}_3\text{PO}_4$  invades

these small pores and establishes the triple-phase boundary also in these regions.

To further elucidate the difference between the Pt/C and  $\text{Pt}_3\text{Co}/\text{C}$ , which are of similar types (Pt deposited on a carbon powder support), and obtain more information about pores between 100 nm and 250 nm, a 3D FIB-SEM image has been recorded. FIB-SEM images of Pt/C and  $\text{Pt}_3\text{Co}/\text{C}$  are shown in the supplementary information in Fig. S5. FIB-SEM images of the Fe-N-C catalyst were previously published by Stariha et al. [19]. The region of interest is shown in Fig. 2b and c. A sample 3D X-ray micro-computed tomogram is shown in Fig. 2b to indicate the hierarchical pore structure. The porous support material exhibits pores in the micrometer range, but the individual carbon flakes shown in Fig. 2c are porous themselves and exhibit pores on the nanometer scale. One such flake was ablated using FIB-SEM to create a 3D image of the nanometer pore space. The resulting pore size distribution is shown in Fig. 2c. The relative frequency analysis confirms the lower amount of small pores in the  $\text{Pt}_3\text{Co}$  catalyst layer. It exhibits more pores with a diameter greater than 100 nm, in which we expect the oxygen diffusion to be faster. The substrate of the  $\text{Pt}_3\text{Co}$  catalyst contains 7% of pores larger than 150 nm in diameter, compared to 1% for the support of the Pt catalyst.

Further, the mean pore size is ca. 83 nm for  $\text{Pt}_3\text{Co}/\text{C}$  and ca. 61 nm for Pt/C. The larger pores facilitate the transport of both the reactant gas and the phosphoric acid. This improves oxygen diffusion by supplying the reactive sites more effectively with oxygen and explains the decrease of the MT in the DRT spectrum. The ORR resistance decrease is defined by the higher intrinsic catalytic activity of  $\text{Pt}_3\text{Co}$  vs. Pt (confirmed by RDE measurements shown in Fig. S2 in the supplementary information) and the improved mass transport, which increases the oxygen concentration at the catalytic sites. Hence, the MT and the ORR correlate.



**Fig. 3.** HFR-corrected polarization curves (a–c) of all three catalysts taken during the conditioning period of the cell, after 2 h (black), after 24 h (red), after 120 h (blue). All cells are conditioned at  $100\text{ mA cm}^{-2}$ .  $U$  represents the cell voltage, and  $j$  represents the applied current density. (For interpretation of the references to color in this figure legend, the reader is referred to the Web version of this article.)

### 3.3. Conditioning of the fuel cells

The cells were conditioned over a period of 120 h. After 2 h and subsequently every 24 h of operation, polarization curves and impedance spectra were recorded. Fig. 3a–c shows the cell performance during conditioning of the fuel cells at  $100\text{ mA cm}^{-2}$ . For the sake of clarity, only three data sets are presented: 2 h, 24 h, 120 h (a complete version of the resistance evolutions is illustrated in Fig. 4). The standard Pt/C cell reached its peak performance (peak performance = within 3 mV of the cell performance after 120 h) after 72 h of operation, whereas the Pt<sub>3</sub>Co/C cell conditioned faster. After 24 h, it already reached its peak performance. The total cell voltage increase during conditioning is higher for Pt/C compared to Pt<sub>3</sub>Co/C. Both cells show similar behavior, as the increase at higher current densities is more pronounced while the phosphoric acid is still distributed within the pores. Initially, the amount of catalyst particles is insufficient to maintain a high current density. This issue results in an additional overpotential at high current density, which is overcome once the acid is distributed more evenly. The Fe–N–C catalyst shows the highest increase in performance. The increase at high current density is especially noticeable, implying that the contribution of the catalyst inside the smallest porosities gradually increases during activation, as a result of their better impregnation by H<sub>3</sub>PO<sub>4</sub>. This explanation is confirmed by Fig. 4, in which the MT resistance and the ORR resistance of the fuel cells during conditioning are shown. The Fe–N–C conditioning is not finished after 120 h of operation, which further highlights the difficulty of phosphoric acid to perchlorate into the catalyst layer. The graphs in Fig. 4 still decrease for both MT and ORR. In the case of Pt/C, the conditioning is finished after 120 h. At this point, the MT resistance and the ORR resistance reach a minimum, and the activation process is completed as the cell reached its maximum performance. Similar values for conditioning time were reported in the literature [59]. For Pt<sub>3</sub>Co/C, the conditioning was already finished after 24 h.

MT and ORR resistances remain at a constant low after this time, and we assume that the distribution of phosphoric acid in the catalyst layer is homogeneous. The variation, as mentioned earlier in pore sizes, can explain this time discrepancy. The large pores facilitate a thorough impregnation. The shape of the DRT spectrum (Fig. S1) confirms that the nature of the internal processes does not change during conditioning of the cells, with the sole exception of Pt<sub>3</sub>Co/C. The ORR peaks of the Pt<sub>3</sub>Co catalyst show a peak growing at 100 Hz–300 Hz. We hypothesize that this peak (allocated to the ORR) might arise due to a change in the surface composition of the alloyed nanoparticles (*i.e.* switch from Pt<sub>3</sub>Co to Pt<sub>3</sub>Co@Pt core@shell [60], Pt-skeleton [61] or Pt-hollow [29]), which alters the nature of the ORR, especially concerning the time constant at which the reaction is taking place. This process is described frequently in the literature [62–65].

The impact of the morphology of the catalyst layer is still palpable after the conditioning of the fuel cells. In the case of the Pt/C catalyst, the MT resistance and the ORR resistance are both higher compared to the Pt<sub>3</sub>Co/C catalyst. This observation indicates that the activity of platinum particles in the nanometer-scaled pores is hampered by the poor H<sub>3</sub>PO<sub>4</sub> distribution and the oxygen diffusion inside these pores. Additionally, the shorter activation phase in the Pt<sub>3</sub>Co/C catalyst case also confirms this. We hypothesize that the non-ideal acid distribution leads to dead zones in the smallest nanometer-scale pores of the catalyst. The nanoparticles are there not in contact with phosphoric acid. Thus, they do not participate in the performance of the fuel cell, even after conditioning. Fig. 5 shows a schematic representation of the phosphoric acid distribution before and after activation. The white background in Fig. 5 indicates the smallest nanometer-scaled areas. For the Fe–N–C catalyst, the Fe–N<sub>2+2</sub> catalyst sites are located dominantly in the nanometer-scaled pores. The activity of these catalytic sites is crucial for high performance, and thus, the impact of the morphology is even more substantial in this type of catalyst. The light blue background indicates smaller nanometer-scale pores (below 20 nm) in contact only after conditioning

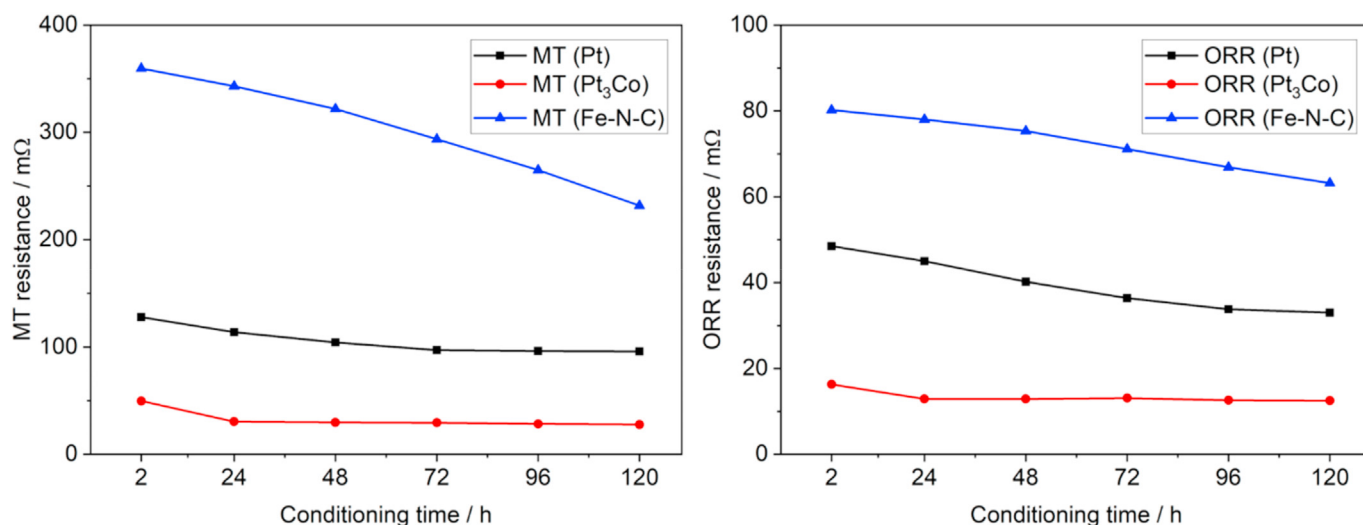


Fig. 4. MT resistance (solid lines) and ORR resistance (dashed lines) for the catalysts during conditioning of the cells. The numbers are obtained from DRT analysis.

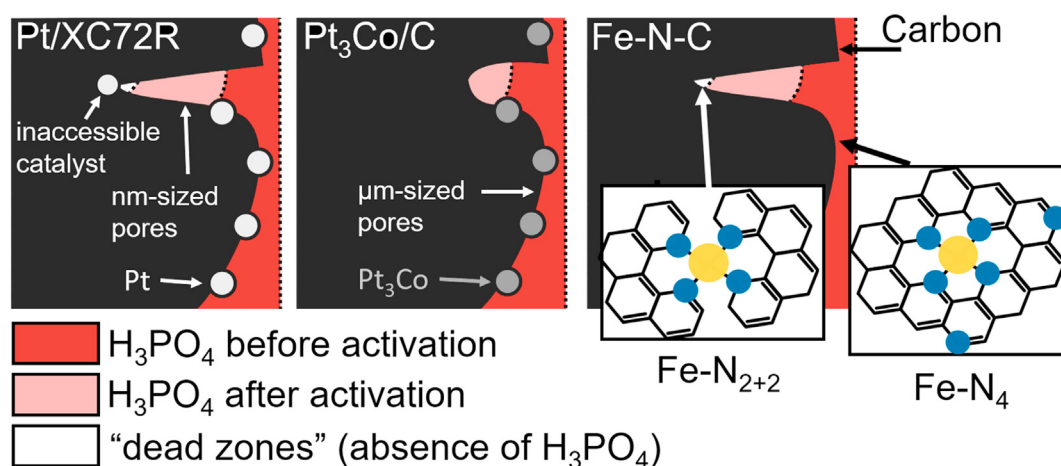


Fig. 5. Schematic representation of the pore space of all three investigated catalyst types during activation. The blue background indicates the phosphoric acid distribution before the activation phase (dark blue) and after activation (light blue). The white background depicts areas in which no phosphoric acid transport is expected. (For interpretation of the references to color in this figure legend, the reader is referred to the Web version of this article.)

and in which catalytic sites are located in all three investigated catalysts. These sites contribute to the cell's performance after conditioning, and they exhibit a substantial MT resistance. The Pt/C catalyst structure includes more of these pores compared to the Pt<sub>3</sub>Co/C system. Thus, the observed MT is higher in the Pt/C system. However, the performance gap is not as significant as the gap of the Fe-N-C catalyst. As the Pt<sub>3</sub>Co/C system exhibits few small nanometer-scale pores, the MT is the lowest. The accelerated conditioning indicates that the wetting of these larger pores with phosphoric acid is facilitated. We assume that more catalytic particles can contribute to cell performance in addition to improved mass transport. The extent to which each effect impacts the performance can not be singled out. Whether an improved wetting in the small nanometer-scale pores or the absence of nanometer-scale pores is more effective in increasing the overall catalyst performance needs to be determined further.

#### 4. Conclusions

This study investigated three different types of HT-PEMFC cathode catalyst: Pt/C, Pt<sub>3</sub>Co/C, Fe-N-C. Each catalyst was implemented into MEA

and characterized by polarization curves, EIS, and DRT analysis. A typical DRT fingerprint pattern is observed for each catalyst type. We found that there is a significant performance gap between these types of catalysts, which can be explained by (i) the intrinsic activity of each electrocatalyst for the oxygen reduction reaction (i.e. Pt<sub>3</sub>Co > Pt > Fe-N-C) and (ii) the morphology of the catalyst layer. The latter was determined by sorption experiments and extracting a 3D pore network from FIB-SEM nanotomography measurements. The conditioning of the fuel cells highlights the impact of the morphology, as the time needed to reach close-to-optimal performances strongly correlates with the phosphoric acid distribution inside the porous catalyst layer. An electrocatalyst with a large average pore size (e.g. the Pt<sub>3</sub>Co catalyst with ca. 83 nm average pore size vs. ca. 68 nm for Pt) facilitates the acid distribution. It shortens the activation period of the fuel cell. The Fe-N-C catalyst experiences the slowest conditioning phase (>120 h), as it requires the H<sub>3</sub>PO<sub>4</sub> to access not only its small mesopores but also its micropores where part of its catalyst sites is found. Through the use of DRT, we were able to deconvolve the contribution of mass transport and ORR kinetics on a given electrocatalyst activity in HT-PEMFC. Therefore, it is emphasizing the fact that mass-transport plays a critical role in the design of such systems.

## Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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## Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.powera.2020.100042>.

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